



ON-DEMAND WASTEWATER LIBRARY

# NUTRIENT REMOVAL

	Nitrogen	Phosphorous
Influent Parameters	<ul style="list-style-type: none"> <li>Expressed as N</li> <li>Total Kjeldahl nitrogen (TKN) = Ammonia-nitrogen (<math>\text{NH}_3\text{-N}</math>) + Organic Nitrogen</li> <li>Total inorganic nitrogen (TIN) = <math>\text{NH}_3\text{-N}</math> + Nitrite-nitrogen (<math>\text{NO}_2\text{-N}</math>) + Nitrate-nitrogen (<math>\text{NO}_3\text{-N}</math>)</li> <li>Total nitrogen (TN) = TKN + <math>\text{NO}_2\text{-N}</math> + <math>\text{NO}_3\text{-N}</math></li> <li>23 to 69 mg/L as N in influent</li> </ul>	<ul style="list-style-type: none"> <li>Expressed as P</li> <li>Orthophosphate and condensed phosphates are soluble</li> <li>Organic phosphate may be soluble, colloidal, or particulate</li> <li>6 to 8 mg/L as P in influent typical</li> <li>Polyphosphate and organic phosphates converted to orthophosphate during biological treatment</li> </ul>
Removal Methods	<ul style="list-style-type: none"> <li>Assimilative uptake for biomass growth</li> <li>15 to 30% N removed by assimilative uptake</li> <li>Biological nitrification, <math>\text{NH}_3\text{-N} &lt; 1 \text{ mg/L}</math></li> <li>Biological denitrification, <math>\text{NO}_3\text{-N} &lt; 5 \text{ mg/L}</math></li> </ul>	<ul style="list-style-type: none"> <li>Assimilative uptake for biomass growth</li> <li>Approximately 1 mg/L P removed by assimilative uptake for every 100 mg/L <math>\text{BOD}_5</math></li> <li>Chemical phosphorus removal, <math>\text{P} &lt; 0.03 \text{ mg/L}</math></li> <li>Enhanced biological phosphorus removal (EBPR) <math>&lt; 1.0 \text{ mg/L P}</math></li> <li>Methods often used in combination</li> </ul>

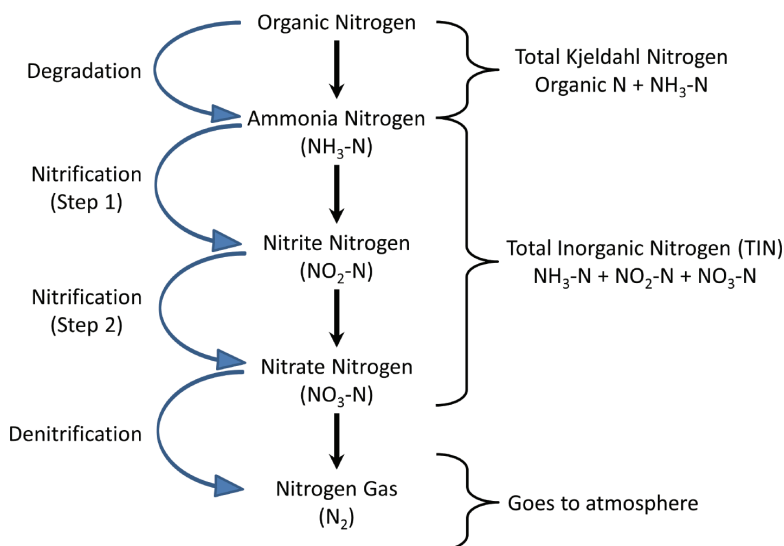
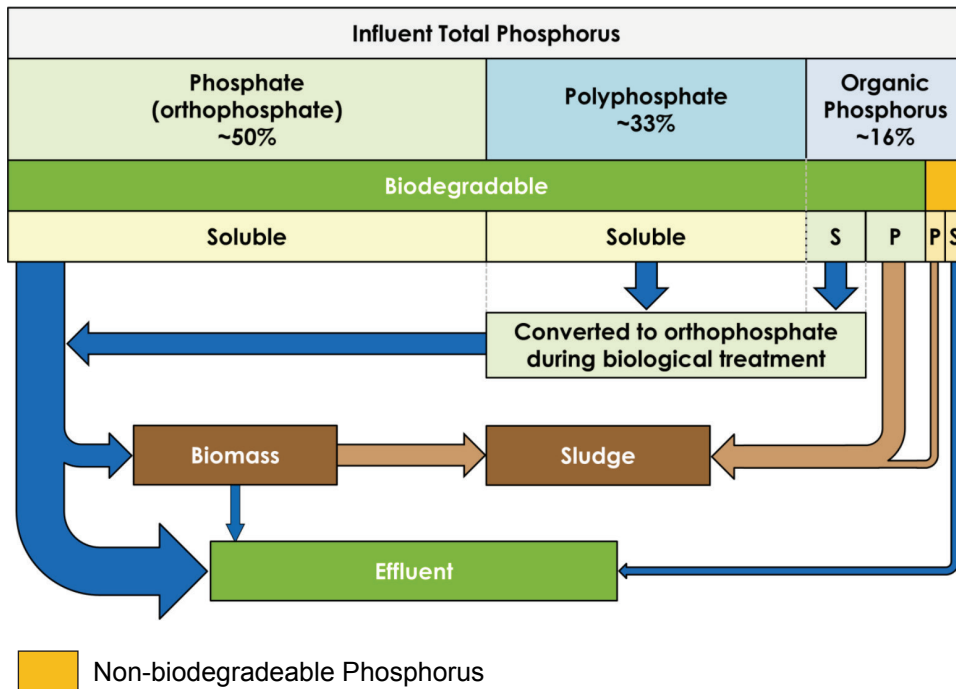


Figure 1 Nitrogen Species in Wastewater



**Figure 2 Phosphorus in Wastewater Treatment (S = soluble, P = particulate; this figure shows the fate of phosphorus in secondary treatment processes like activated sludge unless specific steps are taken to remove it) (Reprinted with permission by Indigo Water Group)**

	<b>Nitrification</b>	<b>Denitrification</b>
<b>Stoichiometry</b>	<ul style="list-style-type: none"> <li>■ Nitrification is a two-step process; the ammonia-oxidizing bacteria (AOB) convert ammonia to nitrite and the nitrite-oxidizing bacteria (NOB) convert nitrite to nitrate</li> <li>■ Converting 1 mg/L of <math>\text{NH}_3\text{-N}</math> to <math>\text{NO}_3\text{-N}</math> consumes 4.57 mg/L of dissolved oxygen (DO) and 7.14 mg/L of alkalinity as calcium carbonate (<math>\text{CaCO}_3</math>)</li> <li>■ The AOB and NOB grow 10 to 20 times slower than heterotrophic bacteria</li> <li>■ Only 0.10 g of new bacteria is produced per g of <math>\text{NH}_3\text{-N}</math> converted to <math>\text{NO}_3\text{-N}</math></li> </ul>	<ul style="list-style-type: none"> <li>■ Denitrification converts nitrate to nitrogen gas</li> <li>■ Many different facultative heterotrophic bacteria can denitrify</li> <li>■ DO concentrations as low as 0.3 mg/L can inhibit denitrification</li> <li>■ Converting 1 mg/L of <math>\text{NO}_3\text{-N}</math> to nitrogen gas (<math>\text{N}_2</math>) requires 4 mg/L of influent five-day biochemical oxygen demand (<math>\text{BOD}_5</math>) and generates 3.57 mg/L of alkalinity as <math>\text{CaCO}_3</math></li> <li>■ Nitrate produced is the equivalent of 2.86 mg/L of DO when recycled to an anoxic zone</li> <li>■ Methanol and other organic compounds increase the amount of nitrate removed; between 2.7 and 3.3 mg/L of methanol is needed for every 1 mg/L <math>\text{NO}_3\text{-N}</math></li> <li>■ Denitrification reduces sludge yield</li> <li>■ Yield depends on carbon source</li> </ul>

	Nitrification	Denitrification
Process Variables	<ul style="list-style-type: none"> <li>■ The aerobic solids retention time (<math>SRT_{\text{aerobic}}</math>) is the most important process control variable for activated sludge processes</li> <li>■ SRT is highly temperature dependent</li> <li>■ Organic loading rate (OLR) is the most important variable for fixed-film processes</li> <li>■ Soluble <math>BOD_5</math> must be less than 15 mg/L for nitrification in biofilms</li> <li>■ DO concentrations of 2 mg/L help ensure maximum nitrification rates in activated sludge processes</li> <li>■ Low DO may cause nitrite lock</li> <li>■ Nitrification rates are highest between pH 7.5 and 8.0, but nitrifiers can acclimate to lower pH</li> <li>■ pH inhibits nitrification by limiting the availability of un-ionized ammonia (<math>NH_3</math>)</li> <li>■ A minimum alkalinity concentration of 50 mg/L as <math>CaCO_3</math>, and preferably 100 mg/L, is needed to prevent pH drop</li> <li>■ AOB can't store ammonia and don't grow quickly enough to take advantage of transient ammonia loads</li> </ul>	<ul style="list-style-type: none"> <li>■ Denitrification is limited by the availability and type of organic carbon</li> <li>■ Anoxic tanks or zones contain nitrate but no oxygen</li> <li>■ Nitrate is produced in areas with aerobic conditions and must be returned to areas with anoxic conditions</li> <li>■ The specific denitrification rate (SDNR) is how fast denitrification occurs</li> <li>■ SDNR depends on the organic carbon to nitrate ratio</li> <li>■ The higher the food-to-microorganism ratio (F/M), the faster denitrification will occur</li> <li>■ Denitrification is faster with soluble BOD than particulate</li> <li>■ Pre-anoxic zones denitrify faster than post-anoxic zones because more organic carbon is available</li> <li>■ Activated sludge processes with a single anoxic zone or basin can achieve total effluent nitrogen of &lt;10 mg/L as N or up to 85% removal of the total oxidizable nitrogen in the influent</li> <li>■ Increasing the internal mixed liquor recycle (IMLR) will increase nitrate removal when organic carbon is available</li> </ul>
Process Control	<ul style="list-style-type: none"> <li>■ Retain biomass in the process long enough to allow the nitrifying bacteria to reproduce and build a stable population</li> <li>■ Use safety factor to prevent moving above and below the minimum <math>SRT_{\text{aerobic}}</math> required to prevent nitrite accumulation</li> <li>■ Reduce competition from heterotrophic bacteria by minimizing organic loading rates</li> <li>■ Ensure adequate supplies of ammonia, DO, and alkalinity</li> <li>■ Manage recycle streams to keep ammonia loading as consistent as possible</li> </ul>	<ul style="list-style-type: none"> <li>■ Add supplemental BOD to maintain a BOD to <math>NO_3</math>-N ratio of at least 4:1</li> <li>■ For activated sludge processes, increase the IMLR to decrease effluent <math>NO_3</math>-N</li> <li>■ Recycle ratios typically less than 400% of influent flow</li> <li>■ Ensure the anoxic zone remains anoxic by minimizing DO recycled in the IMLR and return activated sludge</li> <li>■ Keep anoxic zone oxidation–reduction potential (ORP) between 250 and 150 mV</li> <li>■ ORP readings are dependent on electrode type and fill solution used</li> <li>■ For fixed-film processes, increasing recycle flow increases denitrification</li> </ul>

# Chemical Precipitation

## Stoichiometry

- Metal salts combine with orthophosphate ion to form insoluble compounds that come out of solution (precipitate)
- Aluminum sulfate (alum), ferric chloride, and sodium aluminate are the most commonly used chemicals for phosphorus precipitation
- Weight ratios are calculated from balanced chemical equations; the stoichiometric dose to precipitate of 1 mg/L of phosphate as P requires
  - 0.87 mg/L aluminum ions, or
  - 1.8 mg/L ferric iron ions, or
  - 9.6 mg/L alum, or
  - 2.64 mg/L sodium aluminate, or
  - 5.24 mg/L ferric chloride
- Side reactions consume aluminum and iron ions by forming hydroxides
- To reduce effluent P to 1 mg/L, 1.5 to 2 times the stoichiometric dose is typically needed
- To meet ultra-low effluent P limits, 6 to 7 times the stoichiometric dose may be needed
- Chemical precipitation increases sludge production

## Process Variables

- Aluminum and iron addition consumes alkalinity (mg/L as  $\text{CaCO}_3$ )
  - 1 mg/L alum consumes 0.5 mg/L
  - 1 mg/L ferric chloride consumes 0.56 mg/L
- Supplemental alkalinity may be needed
- Sodium aluminate increases alkalinity
- Wastewater pH affects the amount of precipitate formed
- Optimum pH range depends on the chemical used
  - Alum – 5.5 to 6.5 SU
  - Ferric chloride – 3.5 to 5.0 SU
  - Both work well up to pH 6.5
- Ferrous iron converts to ferric iron in aerobic processes
- Precipitation in anaerobic processes is best at pH 8
- Improve P removal with rapid chemical mixing and longer contact times
- Iron compounds are added at different locations to achieve different process objectives, including odor and corrosion control, improvement of clarifier performance, reducing struvite formation, and precipitating phosphorus
- Aluminum compounds are used to remove phosphorus and improve clarifier performance

## Process Control

- Perform jar tests followed by full-scale testing to confirm dosing calculations
- Add chemicals as far upstream as possible from the precipitate removal to maximize contact time
- Add polymer as far downstream of metal salt addition as possible
- Control dosages upstream of the primary clarifier to prevent
  - Excessive BOD<sub>5</sub> removal,
  - Excessive alkalinity consumption, and
  - Inhibition of nitrification or denitrification in the secondary treatment process
- Minimize effluent total suspended solids (TSS)

## Enhanced Biological Phosphorus Removal

### Stoichiometry

- MLSS is cycled between anaerobic and anoxic/aerobic conditions to promote the growth of phosphate-accumulating organisms (PAOs)
- *Accumulibacter* and *Tetrasphaera* perform luxury uptake of phosphorus
- Phosphate stores energy as poly-P
- Under anaerobic conditions, poly-P is used to take up volatile fatty acids (VFAs)
- VFAs are stored as poly-β-hydroxybutyrate (PHB)
- Magnesium and potassium ions neutralize phosphate ions and make it easier to pass them through the cell membrane
- Fermentation occurs in the anaerobic zone
- *Tetrasphaera* performs fermentation when ORP is below -300 mV
- Luxury uptake occurs in the anoxic and aerobic zones

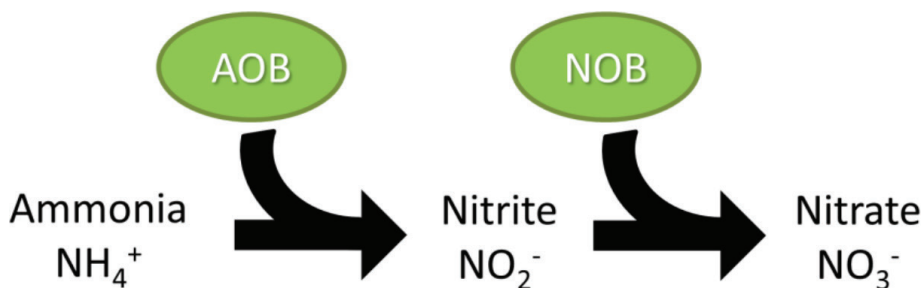


Figure 3 Nitrification Sequence (Reprinted with permission by Indigo Water Group)

## Process Variables

- The organic carbon-to-P ratio is the most important process control variable for EBPR
- Organic carbon must be available as VFAs or readily biodegradable five-day carbonaceous BOD (CBOD<sub>5</sub>)
- VFAs are produced in the collection system and anaerobic zone
- VFAs may also be produced by fermenting sludge in an active primary or other location
- pH below 6.5 in the anaerobic zone inhibits EBPR
- pH below 6.9 in the anoxic/aerobic zones inhibits EBPR
- A minimum SRT of 3 days is needed to maintain PAOs in an activated sludge process

## Process Control

Process control for EBPR includes

- Ensuring an adequate supply and variety of VFAs,
- Preventing DO and nitrate from reaching the anaerobic zone,
- Keeping the ORP below 2300 mV in the anaerobic zone,
- Minimizing TSS in the final effluent,
- Managing recycle loads,
- Avoiding secondary release of P, and
- Minimizing competition from glycogen-accumulating organisms (GAOs)

## References

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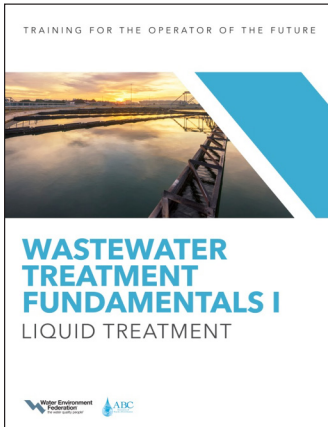
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These peer-reviewed resources represent the expertise of hundreds of water quality professionals. They align with updated Need-to-Know Criteria from the Association of Boards of Certification and are based on WEF's extensive existing resource collection, including *Operation of Water Resource Recovery Facilities*, MOP 11. After learning from real-life examples, users may actively apply the material they learn to situations they encounter in their day-to-day work. The first in the series, *Wastewater Treatment Fundamentals I: Liquid Treatment*, is available as a print manual or as an online course + manual to address different learning styles as well as align with most state CEU requirements. The online course is accessible via desktop, laptops, tablets, and mobile devices.

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